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RESEARCH SOLAR POND: DESIGN AND INSTRUMENTATION

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CENTER FOR ENERGY AND ENVIRONMENT RESEARCH

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RESEARCH SOLAR POND: DESIGN AND INSTRUMENTATION

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ABSTRACT

The Center for Energy and Environment Research (CEER) of the University of Puerto Rico plans to install a 39 m (128 ft) research salt-gradient solar pond. The design, construction and instrumentation of this pond is presented. Drawings illustrate the pond's design and instrumentation methodology. This pond will operate in conjunction with a much shallower evaporative pond of the same diameter. The research pond installation will be used to study automatic and semiautomatic pond operation with the maintenance of the salinity gradient being a main concern.

The basic materials of the pond construction and the sensors and equipment used in the instrumentation system are listed in tabular form. The measurements of principal pond parameters such as brine temperature, ground temperature and moisture, brine flow through the heat exchanger, brine transmissivity and solar radiation are described. The scanning system, the data acquisition system, and the pond operation and maintenance are also discussed,

Salt-gradient solar ponds are large pools of water open to the environment. They are filled with salty water in such a way so that the liquid top layer (upper convective zone) has a salt content of 1-4 percent while the bottom layer (lower convective zone) has a salt content as high as 23-27 percent (see Fig. 1). When exposed to solar radiation, the denser bottom layer heats up to a much higher temperature than the surface layer. The heat accumulated in the lower convective zone is "trapped" by the low salinity nonconvective zone that separates the high density brine at the pond bottom from the upper convective zone. Because heat is stored at the pond bottom, the separate thermal storage normally required in solar installations is not needed.

Since the discovery of natural solar ponds [1], interest in the practical use of pond phenomena has led to the construction

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Fig. 1. Cross-Sectional View of Salt-Gradient Pond.

of salt-gradient solar ponds throughout the world, these activities stimulated work on understanding the physical and engineering problems related to solar pond use [2]. In recent years several laboratory size salt-gradient ponds have been built [3-6].

In our work the design and construction parameters for a 39, n² (415 £2) research pond were established with the view of building and operating a 0.5 acre (21,760 fe) pond to generate industrial process heat in Puerto Alcs in the forures? Fe rand instrumentation package and data acquisition system were deoinced to enable the investigation of automatic or sexiauconacic song operation in maintaining the salinity gradient to isprove thos the presently used methods that call? for manval pond operation and gradient control. Although a computer program for a Ho) Programmable Calculator to determine a pond?s density geadione se available, this manual pond control method is tine congening? and denands the operator's constant attention [1]. the desian aren

blens of the data acquisition and instrumentation package are technically similar to those encountered in solar hestixe aad cooling [ey

2. DESIGN

A number of theoretical models to predict a salt-gradient solar pond's thermal performance have been developed and studied.

A general analytical formulation of the pond's thermal behavior that shows it to be equivalent to that of a flat-plate collector [9,10], the development of a new steady-state analytical method for pond analysis [11,12], and the use of theoretizal eredisone for pond sizing in heating applications [12-15] are some of the approaches that have been taken. A simple method to calculate pond parameters has also been introduced [16], and a number of

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solar pond computer models to predict solar pond thermal behavior in different situations have also been proposed [16-25],

?The thermal efficiency of salt-gradient solar ponds strongly Depends on both brine transmissivity and heat loss to the ground. The solar pond has to be designed then in such a way as to minimize the heat losses from the pond and the wetting of the soil

around and underneath the pond. Wetting is basically caused by ground water movement, rainwater, or brine leakage. Keeping these factors in mind, the preliminary design of the pond was performed by using the simplified method of M. Edesses et al. (16).

These calculations were later followed up by a more elaborate computer analysis that employed the model developed by J. B. Davila Acarón [20]. In addition to the refined steady-state analysis of A. Rabl and C. F. Nielsen [13] his model also takes into account the edge heat losses, bottom heat losses and the effect of surface mixing on the pond's thermal performance.

Figure 2 shows a conceptual drawing of CEER's research salt-gradient pond. The drawing indicates the three distinctive

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zones formed in the pond: the upper convective zone, the non-convective zone and the lower convective zone. The upper convective zone caused by wind stirring and surface heating and cooling is kept as thin as possible, 0.1-0.4 m (0.3-1.3 ft) in research ponds. The lower convective zone's thickness depends on the use of the pond. It is typically 0.5-0.8 m (1.6-2.6 ft) thick, with thicker zones occurring in ponds used for large heat storage. The non-convective zone's thickness depends on a number of parameters and is usually 0.2-1.0 m (0.6-3.3 ft) in research ponds

3. construction

The 7 m (23 ft) ai

ter pond structure will be constructed

by using two 1.2m (4 #

high, commercially available pool

frames one of the other (see Fig. 3). The high sun angle

in Puerto Rico can cause overheating of sloping sidewalls that

significantly increases heat loss via thermal convection along

the walls and promotes upward salt transport by convective mixing. This problem was severe in a production pond built in Alice Springs in Northern Australia [26]. Thus, the CEER research pond walls and their supports, made of galvanized steel coated with a rust-resistant acrylic enamel finish, will be vertical. The pool comes with its own 14-gauge vinyl liner with electronically welded

Soil from the excavation piled around the entire pool will form a berm about 0.9-1.2 m (3-4 ft) high. Since the brine depth is about 1.8 m (6 ft), this leaves 30 cm (1 ft) at the top of the structure for overflow or the adjustment of zone thickness, and 30 cm (1 ft) at the bottom for sand and thermal insulation

A layer of sand a few centimeters thick will smooth the bottom

ground irregularities and protect the Liner from sharp stones in the ground.

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to reduce heat losses from the pond, 10 cm (4 in) thick styrofoam thermal insulation is used on the side walls of the pond and 5 cm (2 in) thick urethane board is used on the bottom. The wall thermal insulation extends 0.9-1.2 m (3-4 ft) beneath the pond bottom to reduce edge heat losses that can amount to up to 30 percent of the heat collected. A vapor barrier will be installed between the wall thermal insulation and the soil.) The primary liner used in the research pond is the Shelter-Rite Hypalon XR-SSP, custom cut and factory welded to fit the pond shape. The secondary back-up liner used is a 30 mil thick PVE liner,

The research pond will be operating in conjunction with an evaporative pond of the same diameter as the research pond, but with a depth of only 1.2m (4 ft). The evaporative pond will have a single layer hypalon XR-5SP liner and thermally insulated walls. To reduce thermal interference between the ponds, they will be built at a distance equal to the pond diameter from each other. The highest ground available on the site was selected for the ponds' construction to reduce heat losses through rain water accumulation in the soil around the ponds. Soil thermal conductivity at the pond site is expected to be up to 2-5 Watts/mec, The pond construction is planned for FY 1984. Table I lists some of the materials selected for the construction.

Table I, Description of Selected Materials.

Material | Model/Type | Quantity | Company

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Styrofoan Board | 1.2 = x 2.4 m Conds

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thermocouple with Porseiny? | 300m] Snes zee

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INSTRUMENTATION

The most important physical parameters of a salt-gradient solar pond are the temperature and salinity gradients. An accurate and efficient system must be designed to monitor these two parameters. Since the CEER pond will be used for research, an elaborate instrumentation system was designed. The system will measure temperature and salinity gradients in the pond, solar radiation at the surface and at any depth, the heat losses to the ground, and the amount of heat energy extracted; it will also detect the presence of leaks in the pond liners.

The measurement of solar radiation at the surface and at various depths of the pond allows the calculation of the solar energy absorbed and provides a measure of the brine clarity. This measurement, with those through the sides and bottom, of energy removed by losses Q_L , and of temperature and salinity gradients will allow the heat balance and pond efficiency to be calculated.

A weather station near the pond will measure ambient temperature, humidity, insolation and wind velocity. This data will be used to calculate the heat losses from the surface of the ponds

4.1, Measurements

The sensors being used in the measurements are listed in Table 11.

Measurement of the pond parameters

Platinum resistance thermometers,

Selected for measuring the brine tempera-

ture. The system's instrumentation design calls for nine RTDs with

temperature gradient measurement capability every 7.5 cm (3 in)s

They will monitor the non-convective zone temperature distribution

by scanning hourly. RTD probes will also monitor the operation of

the diffuser. T type copper-constantan thermocouples in Teflon

Jackets will be installed in the heat exchanger piping to monitor

the brine inflow and outflow temperatures during heat extraction

from the pond. A pump (preferably brass or plastic) rated at

20 liters/min at zero head end driven by 4 1/2 h.p. electric motor

will circulate the brine in the heat exchanger. A shell and tube

heat exchanger with cast iron shell and conjet-nickel alloy tubes

will be used. T type copper-constantan thermocouples will also

be used to measure the ground temperature around the pond. The

design calls for measurement at intervals of 1.3 m (4-5 ft) hori-

zontally and from .3 to 0.9 m (1 to 3 ft) vertically under the

pond bottom. Altogether thirty-seven strategically located ther-

mocouples will be used (see Fig. 4). The underground thermo-

couples will be scanned daily and the signals will be converted

to temperature readings by a data logger. Figure 5 shows the

technique of installing the underground thermocouples.

A leak detection system was designed and integrated into the pond installation. This system consists of a series of T type copper-constantan thermocouples with lead jackets located between the liners. The sand between the liners is sloped so that the leaking brine will accumulate in the center where a sump pump

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Fig. 4. Location of Underground Thermocouples.

can evacuate it. Although electric conductivity probes could be used in a leak detection system, they require an Ave. bridge circuit. To measure conductivity and such a circuit is not compatible with our data acquisition system. For the same reason, an electric resistance grid could not be used for leak detection in a

Flow measurement. A commercially available flowmeter or the flowmeter described by S. M. Gieman et al. [27] will measure the

flow in the heat exchanger loop. PVC piping will be used with the heat exchanger and the diffuser, the flow in the nest exchanger loop will be measured and processed hourly by the data loggers

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les.

During the operation of the diffuser, the flowmeter signals from the diffuser line will be read sunually hourly at the pond site.

Soil moisture ne Five bouyoucos ympsum soil

blocks embedded in the cand Feiwoen the liners and in the soil

under the pond and around the pond will measure soil moisteres A

Pouyoucos soil moisture meter will be read manually every 24

hours. | A salinity probe can be used with this meter to neasure

salinity valvos up to 1000 p:

here is no ideal method to mea-

pond or to monitor the density

density measurement:

density

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gradient. Hydrometers are the easiest instruments to use to check.

the density, but the density determination process is, the one:

ing and subject to error. According to F. Layman» (28) he

Buoyancy of a submerged object has been used successfully at SERT

in laboratory conditions for trace on site measurements, The

Measurement: requires care, however, and does not allow measuring

portions of the grade without stirring at the pond surface

face. Electrical conductivity is used to determine brine

density are good, but they are subject to salinity and re~

platinizing of the elo. = is desired. Pres-
sure measurement is Ene Sead to large
errors in field congitics : ode require
further development sung inves? nethods such

as the vibrating U-tube, which is of sound

look promising. Taste it? It is suitable for brine

density measurement.

In our research, pond, electrode

conductance meter (51) be tested

and the density gradient

Some (2 in) of pond

2 the brine density values

be done hourly at every

sample will consist of a

Section of PVC tube (1/2" copper-constantan thermocouple and a conductivity probe (OF

Plastic) rated at 1/4 inch diameter will circulate brine

through the probe. The probe is in the

Same horizontal plane from which by the probe. This

electric conductivity measurement taking

brine samples for the brine density with 2 salinometer*,

The measurement procedure calls for samples to be cooled to room

temperature in closed containers. Temperature corrections for

Pond temperature are not. From a jar, An automatic

method for scanning ?lesteie covets values is described by

R. P. Pynn et al, (231

Solar racsacion

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Meter will be used to measure the temperature of the brine in the
convective and non-convective layers. Both data will
be done hourly and given, the temperature gradient
measurements. Solar insolation data will be measured by an
Eppley integrator and printed by a Tigris recorder, The
weather station will measure (Guba) and diffuse insolation every
3 minutes. An encapsulation cell can be used for brine
transmissivity measurements spectral response is flat from
the visible to approximately 1 μ m in the infrared. The response of
this cell is indicated in the short

pyranometer will mea

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galibrated and correction factors determined in laboratory condd=
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the data to the Apple II microcomputer system in the data acquisi-

tion room via short haul calling and answering modems. The

Apple II microcomputer will be equipped with an interface card S232 to accept signals from the micrologger. The list of selected equipment is given in Table tv.

Table IV. Description of Selected Equipment

Instrument Model/Type No. | Company

Fischer Seien=

Conductance Meter Model 32 1} tific

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Bouyoucos Moisture

Arthur i. Thoma:

Meter Model IPK25 1 Philadelphia, Pa,

i ? Digites WT Series U:

Solar Data printer Digital necoraer | 1 &

| ?e Mosel 6240 Dayton, ohio

The Eppley Lab=

Solar Data integrator | model 411 1} oratory ine.

a Kewport, Reis

apple Computer

Microcomputer Appie 1 1] Apple, Computer

Monitors tabs Monitors tabs

Data Logger Model 9300 +) san Diego, Ca.

Flow Technology|

Slave unit 200 Channels 1] ine.

Phoenix, Az.

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Mode prt 1020 | 2| tific, Inc.

I Logan, utah

Campbell Scien=

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?? ? ogen, Utah

5. DATA SCANNING SYSTEM

Figure 6 shows the two-dimensional scanning system of temperature, electrical conductivity (density) and brine transmissivity.

A horizontal cable that stretches across the pond is supported by steel pipes that are driven into the ground and held in position by guy lines. A small measurement probe attached to the cable can be moved back and forth across the pond to scan pond parameters by using the combination of pulleys and electric motors shown in the figure. This underwater probe contains a platinum thermometer for temperature measurement, an electric conductivity

Fig. 6. Two-Dimensional Scanning system.

tivity cell, and an Epply underwater radiometer. Figure 7 shows the pulley and underwater probe arrangement. The scanning system would also include fixed RIDs, underground thermocouples and additional electric conductivity cells, flowmeters and weather station instruments. The scanning would have to be done at the maximum rate needed by any one of the sensors, in this case the fixed rate of the RIDs. Of the data will be discarded by the data acquisition system (Apple 11 microcomputer) until its scanning time is attained, i.e. the scanning might take place hourly but underground thermocouple data will be saved only every 24 hours,

For a typical scanning operation,

the measuring probe could be set

at the bottom of the pond. The
would then begin raising the probe.
Minimize the effect of thermal inertia
The scanning system will then do the =
?The scanning intervals can be done
could be as short as 30 seconds.

ation, the horizontal position of
manually and the probe positioned
electric motor. (or a manual winch)
be at a rate slow enough to minimize
{a (0.3 cm/sec). ?the data acquisition
signal scanning of each sensor
determined according to need. and
The data logger interfaced with

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Pig.

General? View of Pulley and Underwater Probe.

the Apple 11 microcomputer will monitor the
frequency will be scanned as an electric motor: pulls them through
the water, microcomputer will be placed in a loop to
await the data logger's scanning signals. The main advantages of
a two-dimensional cable and pulley, data scanning systems are their
versatility, fairly low cost and very adaptability to small
size research ponds. A drawback of
horizontal cable has a ten
conditions.

ing process. The

under moderate wind

an alternative to the above system is the one-dimensional

Scanning system shown in Figure 2. As shown in the figure, the measuring unit is made of 5 cm (2 in) diameter PVC pipes, the system construction is simple and the cost is low, but the unit can only scan on the circumference of the pond by moving on the pond surface. Figure 9 shows details of the measuring unit construction. This system can be used in conjunction with a fixed or floating

measuring platform, more or less sanually oper
automatically operated cable aad valley system,

ted, or with an

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Fig. 8. One-Dimensional scanning System.

PATA ACQUISITION SYSTEM

A microprocessor should serve as the nucleus of a dedicated data acquisition and monitoring system. Through its parallel input/output ports it can perform several operations such as control data acquisition via pre-programmed scanning, process data, make decisions, execute maintenance instructions, and provide feedback between implemented instructions and data which resulted from their implementation. The main advantage of a microprocessor system is its versatility; this feature will be considered in future research on the automation of pond maintenance and operation.

However, since a data logger was available, it was decided to use it as the system nucleus in association with an Apple II microcomputer. A Monitor Labs 9300 data logger combined with an Apple II microcomputer fulfills the function of a data acquisition system in our case. The data logger has forty channels assigned

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Fig. 9. Detailed View of measuring Unit.

for thermocouple signal input, the twenty channels for R?D input;
gightly more channels could be?added. The Monitor Labs 9300 data
logger accepts two independent scanning rates, is equipped with
time averaging features and has an internal clock and printer,
A200 channel-capacity Monitor Labs slave unit works in tandem
with the data logger. The Apple II microcomputer has 48K memory
and is equipped with a disk drive, a video monitor and an interface
card to the data logger. with the Monitor Labs Apple II
interface, the microcomputer initiates the scanning process of the
data logger and stores the data received. once stored, software
Programs can provide data analysis and gradient modification

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instructions. Figure 10 shows the data

room with the

Monitor Labs 9300 data logger in the forecs

Some disadvantages are inherent in this

tem because the Apple microcomputer car

ger, it can only init

form the scanning must

puter can not override the pre-set sequen

Most purposes all the channels must be re

data discarded 2 yr the seannin

by such an arrangement

that the data logye

electric conduct

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7. OPERATION ANC

A diffuser will :

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Fig. 11. Detailed view of Diffuser.

maintaining the non-convective zone (gradient zone) thickness constant by injecting fresh water at the zone surface to replace evaporative losses, and by injecting concentrated brine near the pond bottom to replace the salt. The salt slowly diffuses upward through the solar pond gradient zone at an average annual rate of about 10 kg/m² (2 lb/ft²). During the diffusion process the upper convective zone slowly gains more salt and the lower convective zone loses salt. Because of the high rainfall rate at the pond site will reduce surface water evaporation losses, it may be necessary to pump surface brine into the evaporation pond, and to introduce only small amounts of fresh water onto the surface to build up the upper convective zone thickness to the design level. Concentrated brine from the bottom of the evaporative pond of free salt in the amount up to 120 kg (264 lb) per month may have to be introduced to the bottom of the research pond to replace the salt that has migrated upward through the diffusion process and been discarded with the surface brine. The salt-gradient maintenance in a pond will be a continuous process.

To combat evaporation losses usually a surface wash in the

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amount of 1.0 to 2.0 cm/m² (0.037 to 0.074 in/ft²) of fresh water Per day is sufficient depending on the evaporation rate and rainfall on that day. Any device used on the pond surface for controlling the upper convective zone must also be effective in reducing evaporation that may be instrumental in causing mixing by convective overturn [31]. One way to control the evaporation rate is to install windbreaks that would act to reduce both surface wind stirring and evaporation. Surface oil films are also being tried in research size ponds on an experimental basis.

Wave suppressing devices will not be used because it is anticipated that wind action will not have a negative effect on the operation of a pond of this small size.

Brine clarity in a salt-gradient solar pond is important because radiation falling on the pond must be able to penetrate through the pond's upper convective and gradient zones to the lower convective zone. Chemical treatment of solar pond brine assures the pond's high transmissivity by controlling the bacteri- is, algae and minerals content in the pond. Controlling the pH level through chemical treatment also minimizes corrosion of

Pumps, heat exchangers, and piping. about 0.5 kg (1.1 lbs) per week of chlorine in the form of sodium hypochlorite and hydrochloric acids will be used to minimize bacteria growth in the pond by keeping the pH level ≈ 6.5 . Weekly brine samples will be taken and pH will be measured by using a pH meter. A diffuser loop will be used to adjust pH at a specific depth of the pond. A small quantity of copper sulphate (~1 kg) will be put in the Pond at the beginning of its operation to control algae growth.

Since mostly dirt, especially sand, will fall to the level of the lower convective zone and stay there, a sand filter similar to the one used in swimming pools will be used. The filter loop will be equipped with a by-pass valve to permit periodic flushing with fresh water. For the research activities described above about 17.5 tons of sodium chloride will be used in the research pond and 5 tons of salt in the evaporation pond. Calcium chloride or a mixture of various salts [32] will be used to investigate the concept of pond coupled dehumidification cooling [33].

8. conclusions

The design, construction, instrumentation and operation/
maintenance of a research salt-gradient solar pond has been des-
cribed to provide a basis for studying pond automation and scal-
ing up. It is apparent that the automation of pond operation and
maintenance has not been addressed adequately and needs to be
studied as an important part of salt-gradient solar pond develop-
ment and application. The use of a dedicated microprocessor should
be planned for future pond automation research to obtain data on
@ pond-microprocessor integrated

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REFERENCES

1. A. Kalecsinsky, Ungarische Warme und Heisse Kocksalzeen als Natuerliche Warmeaccumulatoren, Annales der Physik, Vol. 7, No.4, pp. 408-416, 1902.

2. J. 7. Pytlinski, Solar Ponds: Research, Applications and Development, Proceedings of the 5th Miami Tinternational Conference on Alternative Energy Sources, Part B: Solar Applications, pp. 317-341, Elsevier Science Publishers B.V., Amsterdam, 1983.

3. D. K. Dixit, B. D. Shiwalka and V. M. Dokras, Some Studies on an Experimental Solar Pond, Proceedings of the international Solar Enersy Society Congress, Vol. II, pp. 1073-1077, January 1978, New Delhi, India.

4, Annual Report Number M-43, 1 June 1980 to 31 May 1981, Brace Research Institute, McGill University, Montreal, Quebec, canada #9». Ico,

5. B. Nimmo, A. Dabbagh and S. Said, Salt-Gradient Solar Ponds, Solar Ponds, Sunworld, Vol.S, No.4, pp. 113-114, 1981.

6. R. P, Beldam and J. P. Lane, Experimental Operation of a Small Solar Pond, Proceedings of the Canadian Solar Energy Society

Conference ENERGEX-82, Vol.II, pp. 715-720, August 1982,
Regina, Saskatchewan, Canada.

7. R. P. Fynn and 7. H. Short, Solar Ponds - A Basic Manual,
February 1983, The Ohio State University, Ohio Agricultural
Research and Development Center, Wooster, Ohio.

8. Report of the Conference on Performance Monitoring Techniques
for Evaluation of Solar Heating and Cooling Systems, Part 7
and 11, April 7 and 4, 1978, Washington D.c., Sponsored by
University of Utah through BOE Contract BG-77-S-04-4094,

9. H. Weinberger, The Physics of the Solar Pond, Solar Energy,
Vol. 8, No.2, pp. 45-56, 1964.

10. R. A. Tybout, A Recursive Alternative to Weinberger's Model
of the Solar Pond, Solar Energy, Vol.11, No.2, pp. 109-111,
1967.

ALC. F. Kooi, The Steady-State Salt Gradient Solar Pond, Solar
Energy, Vol.23, No.1-D, pp. 37-45, 1979.

12. P. Kooi, Salt Gradient Solar Pond With Reflective Bottom:
Application to the "Saturated" Pond, Solar Energy, Vol.26,
pp. 113-120, 1981.

IRA, Rabl and C. B. Nielsen, Solar Ponds for Space Heating,
Solar Energy, Vol.17, pp. 1-12, 1975.

14D. L. Styris, O. K. Harling, F. J. Zavorski and J. Leshuk,
The Nonconvecting Solar Pond applied to Building and Processes
Heating, Solar Energy, Vol.18, pp. 245-251, 1976.

---Page Break---

as.

16.

a7.

as.

19.

20.

21.

22.

23.

24.

25.

26.

27,

H.C. Bryant and Ian Colbeck, A Solar Pond for London?,

Solar Energy, Vol.19, pp. 321-322, 1977,

M. Edesess, S. tienderson and T. §. Jayadev, A Simple Design

Tool for sizing Solar Ponds, SERI/RP-351-3478, December 1979,

Solar Energy Research Institute, Golden, Colorado 80401, U.S.- A.

J. R, Hull, Computer Simulation of Solar Pond Thermal Behavior,

Solar Energy, Vol.25, pp. 33-40, 1980

W. T. San, Solar Pond Salt Gradient Instability Prediction

by Means of a Two-Dimensional Hydrodynamic Computer Code, Proceedings

Of the Annual Meeting of the American Association of the Interest

Rational Solar Energy Society, May 26-30, 1982, Philadelphia,

Pennsylvania, U.S.A

Je dull, keV. bin, v. S. Cah, oT. Sha, J. Samal and

?, E Melsen, Dependence of Grotind tlest Loss upon solar Pond

Size end rer imecer avion: Calculated and Experimental

Results, the International Solar Energy Soci=

ety Congress O81, Brighton, Erotand.

J, B, Davila Acarcn, Solar Ponds im ruerto Rico = A Feasibil-

ity Study, Pin por?, April 13, 1981, University of Puerto Rico, Conte ergy anc Eavironment evearch, Solar Divic sion, Mai Puorte Rico 09708, U.S.a.

K. A. Meyer, A one-Dimencionai Medel oi the bynam'c Layer Behavior In?a Salt-ceedient Solar Pon © of the Annual Meetivy of the ?mer.can Section vr tie Jacerautionad Solar Enersy foctery, Hey 7) 1981, Philadelpnia, be sylvaniay U.S.A

¥. 8. cha, We P, Me Sehe setling of Surface Convec

ceedings of bie

pp. 1732-1738, 7

ciety Conference,

ole

iibors

K. aA. ? of Layer

Gradient Solar bond, Li-eR-82-908, Los hi

atory, Los Alunas, flow Mowsee 87545, U.S.A

J. ¥. Atkinson and D. R. F. Nerteman, A wi

Model for Soler Ponas, Solar Fregy, Vol

PP. 243-259, 1982

K Dhingra and i. C. Bryant, rhermal Mode! of a Cylindeically
Symmetric solar Pond, Solar Energy, Vol.it, No.6, pp. 589-595,
1983,

R. B. Collings,
Of the 198: Solar world Congenoa, Puen
Western Australis

olar Pond Project, Proceedings
28720, '2983, Perth,

S. M. Glemen, C. Hallberg, hoe and M. Miller, hn Tnexpen-
sive Non-invasive Flowmeter for Solar Anplications, Proceeds
ings of the i941 Annual Meeting of FS/TSES, Vole4-3, 19. /47=
749, Philacciphia, Pennsyivani

---Page Break---

29.

30.

ae

32.

33.

F. Zagrande, Private Communication, October 17, 1983, Solar Energy Research Institute, Golden, Colorado 80401, U.S.A.

R. P. Pynn, P. C. Badger, T. H. Short and M. J. Sciarini, Monitoring sodium Chloride Concentrations and Density Profiles in Solar Ponds by Electrical Conductivity and Temperature Measurement, Proceedings of the 1980 Annual Meeting of

AS/ISES, Vol.3.1, pp. 386-390, Phoenix, Arizona.

F. Zagrando, A Simple Method to Establish Salt Gradient Solar Ponds, Solar Energy, Vol.25, pp. 467-470, 1980.

S. G. Schladow, Private Communication, December 1983, Center for Water Research, The University of Western Australia, Nedland, Western Australia.

D. Schell and C. M. Leboeuf, The Behavior of Nine Solar Pond Candidate Salts, SERI/TR-253-1512, January 1983, Solar Energy Research Institute, Golden, Colorado 80401, U.S.A.

J. A. Bonnet, Jr., J. 7. Pytlinski and K. Soderstrom, Solar Energy Storage for Cooling Systems in the Caribbean, Proceedings of the Solar Energy Storage Workshop, March 20th25, 1982, Jeddah, Saudi Arabia.

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