

# PRNC108

PRNC 108

PUERTO RICO NUCLEAR CENTER

Excess Reactivities Associated  
with Certain Core Configurations

of the PRNC Research Reactor and  
the Proposed Pool Critical Facility

Dr. Aviva E. Gileadi

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EXCESS REACTIVITIES ASSOCIATED WITH CERTAIN CORE CONFIGURATIONS.

(OF THE PRNC RESEARCH REACTOR AND THE PROPOSED POOL CRITICAL FACILITY

Dr. Aviva E. Gileadi

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istence obtained from Mr. C. W. NESTOR of the

Mathematics Division, ORKL = in run;

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in comput ing the few group cross sections is gratefully acknowledged  
herewith.

?The cooperation of the PRNC - Reactor Division in performing the  
critical experiments is highly appreciated.

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(OF THE PRNC RESEARCH REACTOR ANO THE PROPOSED POOL CRITICAL FACILITY

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with certain core configurations of the

## Proposed PRNC-Pool Critical Facility

computed. The same computational method and the same input data, when used to compute the excess reactivity of a

given core configuration of the PRNC | HW Research Reactor, yield results that agree very well (within 2%) with those measured in critical loading experiments on the same configuration = thus establishing confi =

dence in the validity of the computations reported herewith. (See py

126 16)

One of the objectives is to provide dependable reactor physics data to be

in the sa

ty analysis of the proposed PRNC-Pool Critical Facility.

However the usefulness of the data presented herewith is not limited to the solution of that problem, it is more general than that: The group constants may be used as input data to» ver

ty of calculations concer~

?ning both the PRNC Res

wreh Reactor and the PRNC Pool Critical Facility,

Including calculations of flux distribution, depletion, perturbation etc

The fuel elements to be used in the proposed PRNC-Pool Critical Facility

identical with those used in the PRNC Research Reactor. They are

NTR-type, 18 plate fuel elements containing 10.67 g of 20% enriched U305

powder per plate. For the exact description of the geometry and the materials! composition of these fuel elements reference is made to the

Final Hazards? Summary Report PRNC-37. (see ref. 1)

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The results are presented in the following order

- 1, Computed values of few group constants.
- 2, Computed values of effective multiplication factor ( $k_{eff}$ ) for @ set of configurations of the PRNC Pool Critical

Facility.

Comparison of measured and computed key values for a given

configuration of the PRNC Research Reactor.

1. Computed values of Few Group constants

Two, three and four group constants were determined

following regions

- 12, Standard fuel element

b. Partial fuel element

+ Center well

4. Pure water reflector

The group constants were calculated at the Computing Center of Brookhaven National Laboratory, using the HAMMER-code which was developed at ONL. HAMMER contains THERMOS library for thermal and MUFT

Library for fast microscopic cross sections; the rest of the necessary input data describe the materials composition and the geometry of the region. HAMMER-computed few group constants by regions and by energy

Groups are

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Effective miltiplication-factors were computed on the Control Data

e 16OK-A computer of the ORNL Mathematics Division, using "TWENTY GRAND",

4 few group, few region diffusion code developed at ORNL.

Four groups were us

The core configurations chosen include the pro=

¥ Posed basic configuration of the Pool Critical Facility as well as

: certain other configurations of the sane facility obi

ined by a

ing

fone, two, three or four standard fuel elements to the basic configura-

tion, Into the corner positions. Some of these configurations were

Instrumental In determining the excess reactivity associated with the

accident, agreed upon In the case of the PRNC-Pool!

Critical Facility as inadvertently dropping

tendaré fuel element

Into a corner position.when the core Is alrandy critical in its basic

configuration.

?The configuration cat

1d NCONTROL CASE" refers to the actual configuration

\ Of the PRNC Research Reactor used in a critical loading experiment.

TWENTY GRAND calculated effective multiplication constants, together

with the configuration diagrams are given in figures | - 5.



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Pecos

LEGEND

BBB sre.0mo rue. [wate nersscron

∅ EEE cowmo. ve.

. E1gue 1

CORE CONFIGURATION A, COMPUTED Kegs = 1.0143652

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## LEGEND

BBB srmonen ree [J wien nesccton

EER conraon ven

EguRE 2.

CORE CONFIGURATION 8, COMPUTED kay = 1.0212336

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%

OPS

eS

BBB stavonwo ruer [J wares nervecron

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Leceno

BBQ seo rue (te rercecron

FEES) comrnnon wer

FIGURE 4. CORE CONFIGURATION D, COMPUTED  $Kygy = 10341291$

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## LEGEND

+ BRP samo ruet connot weue

: PARTIAL FUEL (1 saves aercecroa

## FIGURE 5. CONFIGURATION ?CONTROL CASE?

couputeo °2029783

ROSES Reve 22

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### 3. Comparison of Measured and Computed Dats for the ?CONTROL CASE:

Im order to check the overall validity of these computations a comparison was made with experimentally determined results. A set of critical loading experiments were performed n the PRNC-Research Reactor

Core in the open pool position and the excess activities were determi-

Used with the aid of a calibrated regulating rod and one calibrated shimrod, The regulating rod was calibrated by the stable period method and the shimrod by the trading method.

Integral calibration curves of the regulating and of the shimrod are shown in Figures 6 and 7 respectively.

Figures 8 through 11 show the core-configurations for which critical loading has been performed.

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File

20304

ROD POSITION (% OUT?)

' REGULATING ROD CALIBRATION CURVE

INTEGRAL RODWORTH VS ROD POSITION

8030100

Figure 6

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20 30 3080

6070

ROD POSITION (%)

PARTIAL ROD CALIBRATION CURVE OF SHIMROD #3

INTEGRAL RODWORTH VS ROD POSITION

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CONTROL CASE ~ MEASURED

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Figure 10: CONFIGURATION H

SH) SH-2 SH=3 Sia RR

100. 100. 100. 100, 36.49

Conditions of one standard fuel

element in lattice position 50

0 the "CONTROL CASE" core results

In 33. excess reactivity - as it

can be read off from the calibration

curves.

+ Rod positions at criticality

<| SH-1 SH-2 SH-3 SH-b RR.

D

100. 100. 23.9 100. 100.

Addition of the last fuel element

SZ

v\)

?amounts to an addition of \$1.75

Ry

Of reactivity = as can be read

Off the calibration curves of the

regulating rod end shinrod #3.

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The discrepancy between measured and computed kerf values in the CONTROL CASE is .0029, which is very satisfactory especially if one takes into account that the computations refer to a clean core and the measurements

were performed on a core that has had an operating history of approximately

80 megawatt days.

Conclusions,

1. From the close agreement obtained between measured and computed values

We conclude that using the BNL-HAMHER code for generating few group Constants and the ORNL-IVENTY GRAND code for determining the effective multiplication factor leads to valid computed results. In an attempt

to corroborate

this conclusion further calculations are being made on

2. We have seen that for configuration A of the proposed PRNC Pool

Critical Facility we obtain a computed  $k_{eff} = 1.014$  corresponding to

clean cold excess reactivity of

this value

by substituting partial fuel elements for some of the standard elements preferably in the center of the core.

3. The excess reactivity associated with the postulated maximum credible accident is computed as the difference between the  $k_{eff}$ 's of cases

and 8.

OK \* 0,0068684 ~ 90g

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## References

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, Research Reactor, 1965, PRNC 37.
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