

PRNC160

PRNC. 160

PUERTO RICO NUCLEAR CENTER

COMPUTER AIDED DECOMPOSITION OF GAMMA SPECTRA
EMITTED BY CERTAIN RADIOACTIVE NUCLIDES

By

Aviva E. Gileadi and Nallagounder Kuppusamy

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ersity of Puerto Rico

Mayaguez Campus

COMPUTER AIDED DECOMPOSITION OF GAMMA SPECTRA
EMITTED BY MIXTURES OF CERTAIN RADIOACTIVE NUCLIDES

by

Nallagounder Kuppusany

A thesis submitted in

partial fulfillment of the

requirements for the degree of

Master of Science

(Nuclear Engineering)

January 1973,

Approved:

af a Wa leeed Rey 1692

airman Graduate Committee a

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ABSTRACT

A computer code PRGA, written in FORTRAN IV, has been developed in order to perform decomposition of certain gamma spectra obtained by means of Ge(Li) diode equipped multichannel data acquisition system. The code uses spectra of the individual standards and those of the mixtures as input data and calculates the mixing factors pertinent to each component, using Linear least squares fit techniques.

PRGA is presently operative on both the IBM-360/40 and the PDP-DEC-10 computers at the Computer Center of the University of Puerto Rico, Mayaguez Campus. The code includes corrections designed to account for deadtime losses, natural

and spectral background, decay and counting statistics. Using source mixtures with premeasured mixing factors, specially prepared for the purpose of comparisons, it was found that the premeasured and PRCA computed mixing factors are in satisfactory agreement.

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and making it operative.

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CHAPTER I

INTRODUCTION

During the last decade or so the development of lithium

é drifted germanium detectors requiring cryogenic techniques and associated low noise electronics and the use of such detectors with various sophisticated data acquisition systems, featuring such items as multichannel analysers with large memories, often interfaced with digital data processors - made a considerable impact on experimental photon spectroscopy.

Improvement of the experimental techniques resulted not only in higher accuracy, and better resolution, but also in an unprecedentedly large quantity of available gamma spectral data. In order to match the efficiency of data acquisition to that of converting these data into meaningful information: numerical techniques are required.

Such techniques not only provide considerable savings in time but also significantly improve the accuracy of data analysis.

Ideally even the most complex spectra should be analysable, qualitatively as well as quantitatively, with little or no man-machine interference. However, before such rather ambitious objective could be achieved, several simpler partial programs need to be developed and checked out, each of them designed to perform a partial task in the framework of

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complete analysis. Once all the partial programs are operative, they are integrated into a complete system, capable to determine background, to resolve and fit complex peak groupings, to determine the energies and intensities of the gamma rays as well as the amount of source nuclides within the analysed mixture.

The Nuclear Engineering Department of the University of

Puerto

Rico, recently acquired a high resolution gamma detecting system consisting of a lithium drifted germanium detector, (manufactured by Princeton Gamma-Tech) to be used in conjunction with a multichannel analyser (model No. 88-015 manufactured by Nuclear Data, Inc.). This system is to be used in a rather extensive neutron activation project planned by the Department.

It is felt that a reliable and efficient computer code-

written especially for analysing data,acquired by the above described, Ge(Li) diode equipped,gamma spectrometer would be a welcome contribution to the departamental efforte in the field of neutron activation.

With this general objective in mind, and as a first step towards it - in the present thesis a computer code PRGA was developed that is capable to decompose gamma spectra emitted by certain source mixtures

PRGA is written in FORTRAN IV and is operative on the IBN-360/40 Computer at the University of Puerto Rico, Mayaguez Campus Computing Center. The code has been tested

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on gamma spectra en!

?ted by several different preneasured source mixtures and its performance has been found satisfactory.

#11 gamma spectra used in testing the PRGA code were acquired by means of the Ge(Li) diode equipped gamma ray detector system of the Radioecology Division of the Puerto Rico Nuclear Center, the description of which is given in

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CHAPTER

REVIEW OF LITERATURE

Gamma ray spectrometry is among the most versatile, most important and most frequently applied methods of modern science, accordingly, the professional literature pertinent to that subject cannot be exhaustively reviewed within the scope of the present thesis. An attempt is made, however, to briefly review a selected set of outstanding original papers on the subject of computerized decomposition techniques ("Yunscrambling") of gamma spectra.

J. MILLS (1) has developed a computer program AUTSPAN for analysis of complex gamma spectra obtained with Ge(Li)

detectors. The program contains options for data smoothing, peak location and determination of peak parameters.

G. D. ATKINSON Jr., J. B. WHITWORTH and S. J. GAGE (2) have written a code, NAA, which seeks out peaks, locates the peak maxima, predicts Compton knees, single and double escape peaks and identifies the unknown nuclides present. The code is written in FORTRAN IV and operative on the CDC-6600 computer.

JEAN KERN (3) after a review of the most accurately known gamma calibration lines, presented a method of obtaining new secondary standards of similar precision, but extending to higher energies. Her method uses simultaneously pair peak method, energy combinations and experimental non-

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Linearity curves.

W. C. WHITE, M. B. SHAPIRO and A. W. PRATT (4) applied Linear programming to decomposing spectra.

J. T. ROUTH and S. G. PRUSSIN (5) have written a For

A program which searches and fits the single and multiple peaks. In addition their code performs the energy, efficiency, Line shape calibration, and error estimates.

The program given by R. GC, HELMER, R. L. HEATH, M. PUTNAM and D. HI, GIPSON (6) computed the gamma ray energies and intensities and provided an estimate of uncertainty, by fitting the gamma ray peaks to a Gaussian and applying a correction for the nonlinearity of the electronic system, for the data obtained both by NaI(Tl) and Ge(Li) detector systems.

R. GUNWINK and J.B, NIDAY (7) have constructed an elaborate program, GAMANAL, which determines the background, the energies and intensities of the gamma spectrum and the amounts of the source nuclides present in the mixture.

Taking selected channels of data of pulse height distribution F. D, KNIGHT (8) applied the method of simultaneous linear equations to find the abundance of the concerned nuclides present with the knowledge of the component spectra and the composite spectrum.

The computer program, CAUSS-V, developed by R. @. HELMER and M.

PUTNAM (9) locates the gamma ray peaks, determines the peak parameters, finds the gamma ray intensities and energies applying nonlinear least square curve fit for the

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pulse height distribution obtained with a Ge(Li) detector system.

M. CIAMBI, L. DADDI and V. D. ANGELO (10) have fitted the gamma ray photo peaks to a Gaussian, using a maximum probability method and compared the results with those obtained by the least square method.

W. W. BLACK (11) used correlation techniques to locate the photo peaks, he analysed pulse height distributions obtained with Ge(Li), Si(Li), and NaI(Tl) detectors. He also applied this method to data obtained by means of neutron time of flight analysers.

An early paper of J. H. HUBBELL and N. E. SCOFIELD (22) deals with "unscrambling" experimental gamma spectra using

matrix techniques.

WALTER F. BURRUS (13) used Fourier techniques to obtain the "unscrambled" spectrum and has assigned meaningful error-estimates to the results.

a

WEST Jr. and R. JOHNSON (24) discussed an unfolding code for the IBM 650. They described a procedure for removing scale and energy dependency.

R. L. HEATH, R. G. HELMER, L. A. SCHMITTROTH and R. A.

CAZTER (15) used interpolation between experimental spectra, to calculate pulse height distributions obtained by NaI(Tl)

crystal system for sources emitting only one gamma ray.

GEMRKE, J. E. CLINE and R. L. HEATH (16) developed

e method to determine both the relative detection

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efficiency and the Linearity of the Ge(Li) detector system.

+ G. HELMER, R. G. GREENWOOD and R. J. GEHRKE (27) have measured the energies of gamma ray photons from 24 nuclides using a Ge(Li) detector and have applied correction for the nonlinearity of the detector system and for the recoiling nucleus.

MARTE PUTNAM, D. H. GIPSON, R. G. HELMER and R. L. HEATH (18) developed a computer program which performs a nonlinear least squares fit to pulseheight distributions, obtained both from NaI(Tl) and Ge(Li) detector systems. Their program fits the data to their modified Gaussian functions and prints out the peak parameters.

The program described by R. L. HEATH, R. G. HELMER, L. A. SCHMITTROTH and G. A. CAZIER (19) smooths the gamma ray spectra, applies correction to the gainshift of the detector

system and fits the data Gaussians using linear least squares criterion.

H. BABA, H. OKASHITA, S. BABA, T. SUZUKI, HI. UMEZAWA and Hi. NATSUME (20) constructed a program to analyse gamma ray spectra obtained by using a Ge(Li) detector. The analysis is based on the first derivative method associated with a number of peak shape tests. The effects of data smoothing and change in peak width were studied.

K. LOW (71) attempted to find the contribution from known nuclides in a complex gamma ray spectrum, using least squares method.

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FILIPPONE and F. J. MUNNO (22) discussed the influence of deadtime losses on the magnitude and shape of the composite spectrum obtained by means of a multichannel analyser, They presented a relation including appropriate corrections.

R. G. WAGGENER, L. F. ROGERS and P. ZANCA (23) Health Physics published @ matrix method to correct for non Linear energy response of NaI(Tl) spectrometer systems.

R. K. GILLETTE (24) has developed @ computer program for the analysis of neutron activation data containing an option for smoothing gamma spectra.

J. I. TROMBKA (25) developed a least squares fitting technique for the analysis of complex gamma ray pulseheight spectra, synthesizing the polyenergetic distribution from a series of monoenergetic components in the incident beam.

H. P. YULE (26) published an exhaustive review paper for computation of experimental results in activation analysis.

D. D. TUNNICLIFFE and G. E. A. WYLD (27) have developed a code, based on linear least squares, that computes directly the weights of the components in a source mixture.

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CHAPTER T1T

THEORETICAL BACKGROUND

In the literature numerous methods have been described, for computer aided analysis of gamma ray spectra obtained with Ge(Li) or NaI(Tl) detector-systems. In most of these methods the analysis is performed with the aid of calculated or measured response functions corresponding to monoenergetic photons or individual isotopic components of the sample.

The physical and statistical phenomena determining the response of a semiconductor type detector to a monoenergetic gamma photon, incident on it, are quite complex and the accurate fundamental calculation of peak shapes for the purpose of spectrum analysis is quite difficult. For this reason and because the peak shape may be sensitive to small variations in experimental parameters, it is desirable to determine a mathematical representation of the composite spectra directly from measured data.

In order to assign a suitable functional representation, it is important to examine some of the factors that determine the peak shape. The primary factor determining the width of a photo peak is the statistical fluctuation in the division of the observed energy between ionization and heating of the crystal lattice. This gives rise to a Gaussian distribution

is die-

1th. The extent to which

with a small specified u

trivution is reflected upon the experimental data, taken with

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10

a particular system,ie dependent on a number of factors. The material properties and the impurities in the detector affect the charge collection and the electronic noise associated with the leakage current.

The combined effect of incomplete compensation of impurities and incomplete charge collection worsen the resolution

and give rise to low energy tailing of the photo peak. At

low energies the contribution to the resolution from preamplifier noise is important and at higher energies the instabilities of the amplifier and the pulse-height analyser begin to affect the line width, especially when long counting times are involved. Although the use of the digital gain stabilizer can decrease the broadening, the stabilization may itself change the shape of the peak.

Finally random summing of pulses at

high counting rates

broadens the peaks and gives rise to tailing. The continuum under the peaks is due to Compton distribution from higher energy gamma rays and general counting background. Without detailed knowledge of the composition of the spectrum we can only say that the continuum in the short interval under one peak on a cluster of peaks is, except for statistical fluctuations, a continuous smoothly varying function of energy. Such a function can be approximated with « polynomial.

Among the several techniques used in computer aided

Decomposition of complex gamma spectra three major ones will

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na

be discussed briefly, following references § and lit

(a) Linear least squares technique

(b) Non Linear least squares technique

(c) Correlation technique

In the linear least squares technique the pulse height spectrum due to a polyenergetic distribution of gamma rays is synthesized by using 2 series of normalized pulse height distributions, due to either monoenergetic components or to the pulse height distribution characteristic of various single nuclides in the source-mixture. Each of these pulse height distributions is weighted so that their sum is a best fit based upon a least squares criterion to the experimentally determined polyenergetic pulse height distribution due to the Source mixture under consideration.

It is assumed that the data points in a portion of the

experimental spectrum can be represented by a function

which depends on a set of parameters p_i . The purpose of a

least squares fit is to find the value of the parameters,

which minimizes the sum of the squares of the deviations of

the data from the function; that is

$\sum w_j (y_j - f(x_j; p_i))^2$ is

minimized. The y_j are experimental data points, the w_j

are the weights associated with the y_j , and the p_i are

---Page Break---

12

the values calculated from the function used to represent the data. The summation is overall the data points used in the fit.

A necessary condition for R^2 to be a minimum, as a function of the p_j , is that the set of equations

are

?

0 for $k = 1, 2,$

$p_j,$

(3.2)

hold simultaneously for all values of k .

If J is a Linear function of the parameters p_j , the problem is a linear least squares problem, and expressions can be derived for the "best" value of the parameters. However, if the function is not linear in the parameters, no explicit solution of the equations exist. In this case a ne-

thod of "Linearization" may be used.

One such method of Linearization is that of Gauss. This method consists of Linearizing the function with respect to a set of parameters θ , by the use of a truncated Taylor series. Initial estimates, θ_0 , of the parameters must be available in order to evaluate the derivatives in the expression; that is:

$\theta_0 = \theta_0$

$\theta_1 = \theta_0 + \Delta\theta$

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13

plus expressions containing higher derivatives, where the derivatives are evaluated at the initial values of the parameter.

The function $\theta(p)$ is a Linear function of the p , if

all derivatives beyond the first are neglected. This gives

2

$R_n = S_w [y - 699] - \text{SAY } 3.3)$

> af: Hen sp Pk

The conditions which now determine the minimum are given by

$aR/8C = 0$ for $k = 1, 2, 0.8$ (3.4)

this gives as many equations as there are parameters p_j .

The solution of this set of equations can be represented

in a compact form by the use of matrix notation. Let the de-

sired changes in the parameters be given by the vector

$a_p = \text{COP })s \text{ BPy } bPy \text{ as)}$

Let the vector B be defined as:

5 [Dao = P09

0; ~ IPC Blz/ apydene

8)

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Ww

The coefficients of the gp, are represented by a symme-

tric matrix with the elements

cn

The set of equations can now be written

caps p Where AP and P are column vectors.

The solution is $AP = A \cdot 8$, where the matrix $a = c7$,

Since the higher derivatives have been neglected in equation (2.3) this process does not yield the solution of equation (3.2). Therefore, equation (3.2) is solved again with the a_i replaced by $(a_i + \Delta a_i)$. This process is repeated in an iterative manner until all the Δa_i are less than some ϵ such that the iterations stop if $|\Delta a_i| < \epsilon$ for all i simultaneously. At this point the fitting process is concluded for each peak.

In order to apply the non linear least squares method

to

to pulse height distributions obtained by means of a Ge(Li) detector system, the following should be considered: A gamma ray spectrum, obtained with a Ge(Li) detector, coupled to a multichannel analyser, consists primarily of a smooth continuous distribution on which is superimposed a series of

peaks. A portion of this spectrum can be represented by

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as

5+ Dy ty ro)

7

here

¥55 vo3ie*[1 # LGR + 2250; 5)?] G3)

with

Gay

is a line which represents the continuous distributions

In a complex peak the subscript j identifies the Gaussian

in equation (3.9); the powers m , and m , are predetermined,

2

even positive integers. The Gaussian parameters x , (center

of photo peak in channels), y_0 (count at peak or x), Δ , (full

width of peak at half maximum in channels) can be determined

in the fit. The parameters α , and α , which represent the

2 "2

deviation of the photo peak from a Gaussian, can also be de-

termined, The line parameters a (value at first channel in

fit) and b (slope) can be determined in the fit. In some

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1s

cases the a, and a) terms have been used in fitting photo

peaks from NaI(Tl) data, but a Gaussian function i.e.

zo a2)

The correlation technique utilizes the cross correlation

"

$c(r) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T f(t) f(t+r) dt$ co 3.13:

afew :

:

distribution of the complex spectrum). Assuming that

$$a(t) = af(t) + n(t)$$

where a is a constant and n represents random noise and ap-

proximating $f(t)$ and $g(t)$ with a set of discrete values, the

cross correlation function can be approximated as

$$C_{fg}(t) = \sum_{r=0}^{t-1} f(r)g(r-t)$$

where t and r are integers (e.g. channel numbers). or the

purpose of discussion $f(t)$ is referred to as search spectrum,

---Page Break---

a

a(t) the data spectrum and C, as the corre! spectrun.

According to its definition, the cross correlation function is generated by forming the products of f , g , and g , keeping the search function sliding by one unit to the left each time t is incremented by one. Thus C , will have a peak, whenever the peak in the search spectrum overlaps itself in the data spectrum, This fact can be used to localize monoenergetic components in the polyenergetic spectrum. In order to do so successfully, it is necessary to find a method of enhancing the structure in the correlation spectrum; it is also desirable to remove all of the background not associated with the structure, Assuming that the data structure has a form

of

$=f \cdot G(t)$

with b constant it can be seen that

flay, D0 if teem

and Gan

fee, to ar term

where M is the number of points in the search spectrum $f(t)$.

?This accomplishes both requirements, enhancement of the structure and supression of background. Therefore the

expression of C, may be modified to read:

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le

c+ Bete]

A, = Ss,

when applying this method to actual data, certain modifications have to be introduced in order to take care on

random fluctuations. It is clear that the term

Seer

will no longer vanish beyond the structure for data where A

is fluctuating in a statistical manner, However, remembering that the computation of A , as given by equation (2.18), it can certainly be expected that fluctuations of one standard deviation or more would be smoothed out. Therefore the square root of A should be sufficient to suppress statistical fluctuations.

With this in mind, the modified equation for C now reads:

ce D_s : [ewe ve] @as

When applying the cross correlation method to decomposi-

tion of pulse height spectra, the search spectrum is a Gau-

| (3.20)

ssian, therefore

Ylewras ove

---Page Break---

19

where

$p_{am} = \text{abyint } Q_a$

The only input parameters are the window width $\#$ and the F_{ut} , N_g is @ constant.

Figures 3.1 and 3.2 contain the pulse height distributions (ata spectrum) and the pertinent cross correlation functions obtained using appropriate search spectra, plotted on the same @iagram. Figure (3.1) refers to a spectrum obtained by a Ge(Li) detector. Figure (3.2) to one obtained by a NaI(Tl) crystal.

Both figures (quoted from reference 11) illustrate the effectiveness of the cross correlation method in locating

peaks.

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CHAPTER IV

MATHEMATICAL BASIS OF THE PRGA-CODE

The PRCA code is based on a mathematical model using Linear least squares techniques to calculate the mixing factors of a multicomponent spectrum.

In its simplest form, the problem may be formulated in

the following manner:

Given the pulse height distribution spectrum of a source mixture, obtained by means of a certain gamma ray detector system, as well as normalized pulse height distribution spectra of the individual components obtained by means of the same gamma ray detector system, the mixing factors are to be determined,

In order to obtain a numerical solution of this pro-

blem, the following mathematical model is used:

Let $S(I,K)$ denote the count rate in the K th channel
due to the I th isotope

$C(I)$ the T th mixing factor to be determine

$T(K)$ the count rate in the K th channel due to
mixture (given)

T the total number of isotopes used in the
mixture (given)

K the total number of channel used (given)

Under the assumption that $T(K)$ the count rate in the

---Page Break---

23

K th channel due to the source mixture is produced by a linear
combination of count rates corresponding to each component,

$T(K)$ may be expressed as:

$T(K) = \sum_{I=1}^T C(I) S(I,K)$

T

. kK aay

In order to determine the optimal values of the C(I) mixing factors a linear least squares fit is used, searching

for a minimum of the function:

KK

i

5 2

D Do free-[Eecrescevo] 29

i

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with respect of the choice of the C(I) mixing factors. The minimizing C(I) values are determined by differentiating U

with respect to each $C(l)$ and setting the derivatives to

zero. This leads to the system of linear equations of the

Following form:

a_{Lh}

leading to

z_p

$S_{reosses.0} D_{Lew} [Lecco]$

Tr_{Kel}

a)

for $J = 1, 2, \dots, 1T$ cs)

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24

denoting

and

KK

Bevorea.w = ac.07 wn

A

u

Sacsecey = ae we)

TA for Je1,2, 6.12

The solution of the set of this system of equations

one obtains

yields the desired C(l) values.

To execute the above computation of the C(z) values,

@ computer program PRGA was developed. The arrangement of

the card deck and the listing of the program are presented

in APPENDIX I.

PRGA is written in FORTRAN IV, level 19, and is operative for the IBM 360/40 and on the DEC-PDP-10, both at the University of Puerto Rico, Mayaguez Campus, Computer Center.

In order to facilitate the debugging procedure, the PRGA

was tested on a simulated problem, which assumed a source

structure consisting of ten components and data from forty one channels.

After its performance on the simulated problem has been found excellent, PRGA was applied to actual experimental data, and the computed results found to be in satisfactory agreement with premeasured control data.

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A brief description of the experimental equipment and Procedures as well as a detailed comparison of the experimental mixing factors with those computed by the PRGA program are given in Chapters V and VI.

The performance of the PRGA has been improved by the inclusion of several routines for various corrections, The mathematical basis of these routines is briefly presented

below:

a. Dead time correction was taken into account by first including the system dead time as an input parameter then correcting each raw count rate reading

8 in the following wa;

8 (4.9)

ms

where S is the raw count rate per second and is
?the system dead time in seconds. Dead time values
used in this paper were computed from the percent
values automatically recorded by the counting sys-
tem. No attempt was made to include channel and
half Life dependent dead time correction such as
advocated by W. FILIPPONE and F. J. MUNNO (see
ref. 22) in the code, at this stage of its develop-
ment, primarily because all control data referred
to sources with half lives of several tens of days,
thus the advocated correction would be negligible.

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Correction for natural background is made simply by
including the appropriate background count rates

BB(K) as inputs in the program and by replacing

$S(T, K) = S(T, K) - BB(K)$ (4.20)

for $K = 2, 2) 04. KK$

Corrections related to counting statistics. Due to the inherently random nature of radio active disintegration, allowance had to be made for the statistical fluctuations in the count rates. This was accomplished by assigning a weight factor w ,

e

to each value of

u

fra « Secrsosce

modifying the function entering the least squares

fit in the following manner:

«Yh [ro- Frcoren]? wan

é

Correction for Compton scattering was made in a purely heuristic fashion, by deducting the pertinent ordinates of an appropriately chosen linear function from the measured values. Assuming that the peak

occurs at

θ_0 and the tangential points θ at $K-M$

---Page Break---

2

near function to be deducted is

resp. K, θ the

given by

vei + EEO ysraay (wae)

and the proper correction consists in replacing

SCO =? 8(7,10-¥CK) for

KS KM, KML, cess Kottt easy

Admittedly, the nonlinear method of fitting the individual peaks to the sum of a Gaussian and a linear function, as described in Chapter III, is better justified from the theoretical point of view it should be observed, however, that even the above described simple Linear routine is used by several authors

(refs. 5, 9) and that its use in PRGA yielded

satisfactory results.

Decay corrections are necessary when the code is applied in neutron activation analysis involving short Lived isotopes.

In order to understand how this correction has been applied let us consider the time behaviour of a single isotope's activity assuming that

0 to t_y - is the irradiation time

t_y to t , - is the cooling time

t_y to t_y - is the counting interval

---Page Break---

ALG)

28

the activating flux

is the decay constant of the i -th isotope

is the activation (microscopic) cross

section of the nuclide producing the i -th

isotope

the time dependent activity of the i -th

isotope

the time dependent number density of the
i-th isotope and

the number density of the nuclide, the

activation of which yields the i-th isotope.

Under these assumptions the following holds:

Be down agnpcer octet, ww

=

leading to

Neo = Mgef. ost] o<tety was)

during cooling, i.e. when $t < t_c$

uted = BOeifie? Mt] fen Aneta] (w.a6

and during counting, i.e, when $t < t_c$

goo +» MBs e sale

dco] a7)

---Page Break---

The activity of the sample at any instant of the counting

interval is given by: $t, t \text{ ty}$

Ay CDE AN, $(E)=NS a, (1-e?Nita eo? (tty) (wae)$

Therefore the count rate due to the i -th isotope will be pro-

portional to: os

S

va Wait, | ast

[sonaviiefer? joe ee =

, a ws)

Peo b- 4] fewert oer]

Hence in the case of a mixture consisting of short lived isotopes the mixing factors that will result from the least squares fit - described above - will depend upon t_y , t_y ,

t_{ez} and \otimes and in order to get mixing factors characterizing the composition before irradiation, the following cor-

rection has to be applied:

cect

(4.20)

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30

From the mixing factors, $CC(I)$, of the unirradiated sample, the actual weights are computed by using the normalized activities and weights of the corresponding standard samples.

In order to compute the weights of the individual components in the unirradiated mixture, the following basic

equation has to be used:

$w_i = \frac{A_i}{A_{std}} \cdot w_{std}$

where

w_i = weight of component i in the sample

w_{std} = weight of component i in the standard

A_i = activity of component i in the sample

A_{std} = activity of component i in the standard

100 = observed counts in channel K

ϕ = neutron flux

W_J = weight of the J -th isotope in the sample

A_J = specific activity for radioisotope J at
channel K

λ_J = decay factor for radio isotope J .

The validity of the above equation is subject to the
following restrictions:

(a) The number of counts observed for any component
is directly proportional to the amount of the com-
ponent present.

(b) The spectra is additive.

(c) The flux remains constant during irradiation.

(2) The "deadtime" of the data acquisition system does
not change during any counting period.

---Page Break---

?This results in a set of equations equal in number to the number of channels. If the specific activities $A(x,s)$ have been determined by prior calibration, then this set of equations can be solved for the unknown weights $W(x)$ using least square techniques.

a1

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CHAPTER V

EXPERIMENTAL PROCEDURES AND EQUIPMENT

The performance of the PRCA code was evaluated by comparing premeasured mixing factors with those computed by the code.

Standard sources and source mixtures were prepared from a set of liquid reference sources manufactured by Atomic De-

velopment Corp.. The set included the following nuclides:

wucLIDE | MOST PROBABLE ENERGIES | HALF LIFE

Mev

Na²² 0.511, 1.275 2.82 yr.

mn 0.829 200 days

co⁵⁷ 0.122, 0.136 270 days

co⁶⁰ 2.273, 1.392 5.2 yr.

cs¹³⁷ 0.662 30 yr.

In order to ensure adequate accuracy self filling lambda
Pipettes were used for measuring radioactive liquies.

Health Physics regulations and instructions referrin

z to

handling open sources were strictly observed. After receiving

the reference sources, they were tested for leakage by the

---Page Break---

33

PRNC - Health Pysics Division (see copy of leak test report).

All operations involving liquid sources were performed under
a hood, with the experimenter wearing protective gloves.

Standards and mixtures were prepared at the same time in order to avoid errors due to decay. An aliquot of the reference liquid (e.g. S004) was pipetted on a planchet. A multiple of that aliquot was entered into the planchet that was designated to hold the mixture. Care was taken to deposit the liquid at the center of the planchet in order to preserve identical geometry as much as possible. All sources were dried under a lamp and after drying all were covered with thin plastic covers.

All sources were counted on the Ge(Li) spectrometer of the PRNC Radioecology Division.

A block diagram of the counting equipment is shown in Figure §.1 and a list of the components is given below.

Ge(Li) detector and associated data acquisition system

components:

Hv ~ High voltage power supply, manufactured by Hewlett-Packard; model No. 3015.

Ge(Li) - Lithium drifted germanium detector, ma-

nufactured by Canberra Industries Co.;

model No. 7229-240; with cryostat model

No. 7500.

PRE AMP Preamplifier, manufactured by Canberra

---Page Break---

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Us aun01g

W3LSAS NOILISINODY viva

aM

vow

20v

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fuaiam3aAs

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Industries Co.; model Wo. 979,

AMP - Main Amplifier, manufactured by Tennelec;
model No. 70200.

abe ~ Analog to digital converter manufactured
by Hewlett-Packard, model No. 160.

Mea ~ Multichannel Analyzer, manufactured by
Hewlett-Packard; model No. 45.

TYPEWRITER Manufactured by IBM; model No. 11- ϕ .

X-Y PLOTTER Manufactured by Hewlett-Packard; model
No. 7890 ϕ .

The Ge(Li) detector used in this system is of open ended
coaxial pin type. The starting material for the detector is
P type germanium (doped with gallium). Lithium, acting as a
donor is diffused, at high temperature (400 C°) into the

cylindrical ingot creating a thin n-type layer on the surface. A bias voltage is used to cause the lithium ions to drift through the p type material. During this process an equilibrium condition is established where lithium ions pair with atoms of the doping material (gallium) creating an intrinsic region with intrinsic properties. (See Figure 5.2).

The term intrinsic implies that charge carriers will have a very long lifetime with all recombination processes reduced to a negligible level. Under reverse bias the charge carriers can then be collected from this region resulting in the production of a solid state ionization chamber.

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fee

Lithium-Drifted

Intrinsic Region

FIGURE 5.2

(from reference 28)

---Page Break---

37

ber, schematically represented in Figure 5.2.

Since the mobility of lithium ions in germanium is not negligible at room temperature, such devices once fabricated, must be maintained at low temperatures to preserve the structure. A liquid nitrogen filled cryostat was used to maintain the required temperatures.

Figure 5.2 indicates the configuration of the Ge(Li) detector actually used in this project.

On the average only 2.8 eV is required to create an e-

lectron-hole pair in a Ge(Li) detector as compared to 30 eV in a gas filled ionization chamber or to 500 eV required to produce a photoelectron at the photocathode of a scintillation detector system. It is this reduced energy requirement that improves the statistics and thereby the resolution of

Ge(Li) detectors in comparison to gas-ionization chambers or scintillation detectors.

The Figure 5. energy vs. channel number is plotted, indicating excellent linearity of the counting system used for Gata acquisition. Source mixtures and pertinent standards were counted within a few hours - thus reducing errors due to decay. Maximum counting registered by the inbuilt dead-time counter were below 2%. Within each counting session the gain shift remained below observable.

In order to ensure acceptable counting statistics one hour counts were taken. Count-rate outputs were obtained

both on an IBM typewriter and on an X-Y plotter.

---Page Break---

Lithium Diffused Junction

N

8

p-Type Core

Open-ended Coaxial Ge(Li) Detector

FIGURE 5.3

(from reference 28)

---Page Break---

ENERGY I ee

SYSTEM, ENERGY V5. CHANNEL WBE

308

5300 ??eoe

?OMANNEL NUMBER

FIGURE 5.4

300)

?00

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CHAPTER VI

PRESENTATION AND DISCUSSION OF RESULTS

PRCA computed results are presented in tabulated form side by side with premeasured mixing factors in order to facilitate comparison of the two. Entries in Table 6.1 refer to the ten-congonent simulated problem. Tables 6.2 through 6.5 contain results referring to two, three, four and five component source mixtures respectively. Discrep=

5 Of premeasured and PRCA computed mixing factors are

indicated in percents. Figures 6.1 through 6.

are samples
of pulse height distribution spectra of standard sources
and of source mixtures plotted from data obtained by the
Ge(Li) detector equipped data acquisition system described
in Chapter 4.

The excellent agreement between assigned and PRGA com-
puted mixing factors in Table 6.1 indicate that the perfor-
mance of the PROA-code is essentially right. when applied
to experimentally acquired data, which by the nature of the
acquisition are affected by such factors as gainshift, coun-
ting statistics, spectral background, etc., the discrepancy
Of premeasured and PRGA computed results - understandably
enough - increase substantially.

The PRCA computed results presented in Tables 6.2 through
6.8 are including corrections intended to compensate for er-
rors related to background, deadtime, Compton scattering and

---Page Break---

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counting statistics.

Comparable published results quoted from three references are presented in Tables 6.6 through 6.8.

Based upon the results presented above, the following

can be concluded:

(a) The code developed can determine mixing factors of source mixtures, using gamma spectrum of the composite source as well as those of the standard sources as input.

(b) The PRGA-code is operative on the TBM/360-40 and the DEC-10 computer both at the Computer Center of the University of Puerto Rico, Mayaguez Campus.

(c) PRGA's performance on a ten component simulated problem was found excellent.

(a) PRGA computed mixing factors have been found in satisfactory agreement with premeasured values in @ set of measurements performed on two, three, four and five component mixtures - especially prepared from reference source liquids for the purpose of this test.

(e) As indicated by entry 3 in Table 6.3, PRGA gives a near-zero mixing factor for a standard absent from the composite spectrum.

---Page Break---

COMPARISON OF ASSIGNED AND PRGA-COMPUTED MIXING FACTORS

TABLE 6.1

FOR TEN COMPONENT SIMULATED PROBLEM.

MIXING FACTORS

Component [Assigned | PRGA Computed Discrepancy

«©

A 8.20 5.20 0.00

8 7.30 7.19 1.82

c uso 8.51 0.22

> 6.60 6.01 ous

E 20.60 10.62 e.08

F 13.80 13.82 0.07

6 1.wo awe 9.00

a 0.86 0.88 1.6

1 3.80 3.80 0.00 |

x o.us o.us 0.00

---Page Break---

TABLE 6.2

COMPARISON OF PREMEASURED AND PRGA-COMPUTED
MIXING FACTORS FOR TWO COMPONENT SOURCE MIXTURES

43

_MixIne_FacToRS]

SAMPLE DISCREPANCY

NUMBER | componrn | pRca-come. | prewras. ic

aiwa?? 1.19 1.09 10-0

1

ssc5237 2.08 2.00 8.0

27087 2.35 2.5 6.0.

2

axa? 3.27 3.32 1.8

27.087 30.0 8.47 15.3

5 22

wana? 2.0 5.80 15.7

---Page Break---

TABLE 6.3

COMPARISON OF PREMEASURED AND PRGA-COMPUTED
MIXING FACTORS FOR THREE COMPONENT SOURCE MIXTURES

ee

4a

MIXING FACTORS

SAMPLE DISCREPANCY

numeer | compowryr| prempas. | proa-coup. s

aana?? 2 1.86 2.0

1 co8? 1 0.90 10.0

nS 2 2.99 a8

ana? 0.33 0.32 2.0

2 co8? 5.90 5.12 24

270° 9.38 7 23.3

aina?? 3.33 3.09 2.2

3 2700°7 2.5 2.37 5.2

270089 o 0.07 =

---Page Break---

TABLE 6.4

CORPARISON OF PRENEASURED AND PRGA-COMPUTED

MIXING FACTORS TOR FOUR COMPONENT SOURCE MIXTURES

MIXING FACTORS

SAMPLE DISCREPANCY

numpex | component ___| PRENEAS[PRCA=CORE| \$

aina?? 2 1.62 13.0

2stins4 1 0.38 12.0

270089 2 1.95 2.5

sscs137 2 1.60 18.0

aina?? 2 Lieu 18.0

sa 2snins* 1 0.92 8.0,

° 27ø080 2 2.35 2.5

sscgi?? 2 2.61 23.5

* Computed with $w = 1/\text{TOD}$

8 computed with $w = 1/\text{SQRT}(\text{TCO})$

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TABLE 6.5

COMPARISON OF PREMEASURED AND PRGA-COMPUTED
MIXING FACTORS FOR FIVE COMPONENT SOURCE MIXTURES

>

MIXING ACTORS

SAMPLE DISCREPANCY

numpex | compouewa| prewrass.| pRca-coMP. 8

ana? L 0.92 8.00

7 27C087 1 0.76 24.00

oH

25th us 9.37

27C08° 1 2.03 3.00

sscs19)| 2 der 9.50

ana? a 0.93 7.90

aa 27ç087 2 0.79 22.00

2

25rinS* sé 1.7 8.20

27ç08 a 2.03 3.00

ssost37 2 277 22.50

* Computed with $w = 1/TCK$)

** Computed with $uj = 1/SQRTCTCK$)

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4

TABLE 6.6

RESULTS QUOTED FROM REFERENCE
FOR TEN COMPONENT MIXTURE

~ ~ ?Quay PY

2s)

quantity

DISCREPANCY

component | premeasures | compurep \$

ae? 36-8 gm 20.0 ven 3.3

ask? 0.40 mgm 0.303 mgm 25.0

25Hn56 9.202 em 0.090%yem 20.4

zise® ay.2 22.2 yen aan

aaas?® \$.00 4.98 gem oe

aan

een

29cu%* 2.23 wen 211 yen 0.9

on

so

5

2ucrSt 1.82 1.86 ym =34.0

g3x128 2.49 2.68 yen 2.6

s7iat¥ 2.19 3.02 wen 37.8

uana?? | 5.00 ug 17g suo |

---Page Break---

RESULTS QUOTED FROM REFERENCE

TABLE 6.7

@

FOR THREE COMPONENT SOURCE MIXTURES

4B

MIXING FACTORS

DISCREPANCY

coMpoNEnt. easureo | compurep 8

Sacer 1 1.03 2.92

5508137 5.2 5.31 2.07

27C08 5 5.22 2s

---Page Break---

TABLE 6.8

RESULTS QUOTED FROM REFERENCE (6)

TOR FIVE COMPONENT MIXTURE

MIXING FACTORS

DISCREPANCY

component | premeasured | compurep 8

1 1 0.980 1.00

2 2 1.009 0.89

3 1 2.008 0.79

4 a 1.018 2.50

5 1 1.010 0.99

---Page Break---

COUNT RATE PER HOUR

10,000

000

100

GAMMA RAY SPECTRUM OF 37

RADIATION EMITTED BY gac

re)

CHANNEL NUMBER

FIGURE 6.2

E10 662 Mew

300 a8

---Page Break---

COUNT RATE PER HOUR

10,000

GAMMA RAY SPECTRUM OF
RADIATION Emitted BY C8

a a

CHANNEL NUMBER

FIGURE 6.3

720)

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9 3yno14

waennn TaNNEHD

sunset ed

apn" 49 o3L4ma Kouviony

40 mows 3345 A¥Y YARD

senisors

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?now waa aava anno

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os.

\$79 3unoz4

waanw Tae

40 mnaioads Avw vaMvs

?now wad 34¥¥ LNn09

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979 gangs

w30nAN TaNNVHD

coe ozs ons,

096 090 om 0m ooo on

ETT 8

nam saziea

sanzeto-3

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?9 guns

waenAW TaNNYHD

08 008 oz ov) os om oo een

Woon 3 34¥ ANn02

a0 mnioaas Avy eMMYD

san ss90r3

ran 29003,

samo |

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mais ane

san 2990-3 san ziona

now waa au¥y inn0>

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Future plans include both increasing the accuracy and extending of the scope of applicability of the PRGA-code,

The accuracy is hoped to be increased by

a) Establishing a

rery tape on which the spectra of individual standards, obtained with very good counting statistics, will be recorded. Whenever data on an

additional standard spectrum will become available,

1 be entered into the Library tape using an

appropriate format.

D) A baseline and gainshift routine will be added to the existing code. According to Parr and Lueas (31) even a gainshift of one channel may change results considerably.

?The scope of applicability of PRCA is thought to be extended beyond the present one by

(2) Including a routine based on cross correlation techniques for locating peaks.

() Including an option for locating peaks emitted by the same nuclide and assigning them the same intensity.

(e) Applying nonlinear least square fit techniques s.e. to fit experimental points to the sum of a Gaussian and a linear function.

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The ultimate objective in computer aided spectral deconvolution as indicated by several authors (28, 30) is to have a set of activation analysis data fed to the computer and have the computer to determine the composition of the un-irradiated mixture with no further man-machine interference. Better even have the computer continually monitor the output of the spectrometer, computing and evaluating while the counting is in progress, controlling the counting time, so that the sample is counted just long enough to get the desired statistical accuracy and then request the system to change samples.

It is towards those very ambitious objectives that our

future research efforts will be dedicated.

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?APPENDIX,

ARRANGEMENT OF INPUT CARD DECK

FOR PRGA-CODE AND CODE LISTING

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J=

PROA-PROORAM

ARRANGEMENT OF INPUT CARD DECK FOR
PRGA - CODE.

FIGURE A.)

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PRGA-CODE LISTING

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zy

Fee vaeia6)

c

c

¢

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PROGRAM... PRGA

NsKUPPUSAMY NUCLEAR ENGG, DEPT cAAM

DIMENSTON S(i@, 268)

1) +KP (268), ¥(262), +S\$1G(5),D,AM(5).CC(5),Y¥ (288)

DOUBLE PRECISION? 8,1, 1rsx,ayeRSCAR~0.B AUK

THIS ?pRoGRaM ComPUTES THE? WEXING FACTORES.C(11.QY LEAST SoUARE FI

Lf SPECTRA OF THE COMPONENTS ARE GIVEN AS INPUTS

S8(1o4) 18 THE KeTH ORDINATE OF THE T-TH SOURCE

Hie

Siw

321 FORMAT('L THE NUMBER OF COMPONENTS #tL4s/'2 THE NUMBER OF POINTS.

iy i

Ti 1S _THE NUMBER OF SPECTRA CONSIDERED ~?

ee 18 The UNGER OF POTATS PER SBP TRON

REAQ(2 +200) (CSC 1K) e 184611) KRDO KK)

aoe PARAS SS

grecse2es ,

dee FonmAt 82 801 RY=VALUEST/79

WRITE (3+ 223) (SC 1 eK) L2de11) Keds KK)

2es Fommat(Gneyseer)

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300 Fornaftare:

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333 Pommard fw =vALUESI7/779

UTE ase too _

S34 FokmaT ings oree 35

EACKGROUND AND DEAQTIME CORRECTIONS OF DATA _ ao

READ(2,386)(BB(K) KEL KR)

106 FORMAT, >

READ(2. 402) TAU

402 FoRMAT(F7.2)

WaTTECS.86)

8 FORMATS VALUE OF TaUty/>

WO RRITE CS, 95) 74U, ?

95 FORMAT CAM

0-483 i=2,

00 403 Kei sKK

2.2)

SCR SSCL RCE CT RVETAUTY

SUL) 28C144) -88(K) ae

CONTINUE

00104 K=2.4

TOS ETO /L= CRYATATIY

TOR) ET CK 88K)

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COMPTON CORRECTION

HOTS waLFMroT

REQ(2.203)HC, KKP.

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